

# Generalized Eigenvalue Problem in FEM Modelling of the Resonance Frequencies Piezoelectric Resonators

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- \* large sparse linear algebraic system, which defines the generalized eigenvalue problem
- resonance frequencies are subsequently found by solving this algebraic problem
- typically, we are not interested in all eigenvalues (resonance frequencies)  
⇒ for determining of several of them we consider iterative methods

# Physical formulation

linear piezoelectric constitutive equations:

- generalized Hook's law

$$T_{ij} = c_{ijkl} S_{kl} - d_{kij} E_k, \quad i, j = 1, 2, 3, \quad (1)$$

equation of the direct piezoelectric effect

$$D_k = d_{kij} S_{ij} + \varepsilon_{kj} E_j, \quad k = 1, 2, 3. \quad (2)$$

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symmetric stress tensor  $\mathbf{T}$ , symmetric strain tensor  $\mathbf{S}$ ,  
vector of intensity of electric field  $\mathbf{E}$ , vector of electric displacement  $\mathbf{D}$

$c_{ijkl}$ ,  $d_{kij}$ ,  $\varepsilon_{ij}$  ... material tensors ( $c$  is symmetric in all four indices and PD,  $d$  is symmetric in last two indices and  $\varepsilon$  is symmetric and PD)

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$$S_{ij} = \frac{1}{2} \left[ \frac{\partial \tilde{u}_i}{\partial x_j} + \frac{\partial \tilde{u}_j}{\partial x_i} \right], \quad E_k = -\frac{\partial \tilde{\varphi}}{\partial x_k}, \quad i, j, k = 1, 2, 3,$$

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- governing equation for piezoelectric continuum

$$\varrho \frac{\partial^2 \tilde{u}_i}{\partial t^2} = \frac{\partial \Gamma_{ij}}{\partial x_j} \quad i = 1, 2, 3, \quad x \in \Omega, \quad t \in (0, T), \quad (3)$$

$$\nabla \cdot \mathbf{D} = \frac{\partial D_j}{\partial x_j} = 0, \quad (4)$$

with density  $\varrho$ , volume of the resonator  $\Omega$  and its boundary  $\Gamma$ .

# Physical formulation

• (1) + (2) + (3) + (4)  $\Rightarrow$

$$\rho \frac{\partial^2 \tilde{u}_i}{\partial t^2} = \frac{\partial}{\partial x_j} \left( c_{ijkl} \frac{1}{2} \left[ \frac{\partial \tilde{u}_k}{\partial x_l} + \frac{\partial \tilde{u}_l}{\partial x_k} \right] + d_{kij} \frac{\partial \tilde{\varphi}}{\partial x_k} \right) \quad i = 1, 2, 3, \quad (5)$$

$$0 = \frac{\partial}{\partial x_k} \left( d_{kij} \frac{1}{2} \left[ \frac{\partial \tilde{u}_i}{\partial x_j} + \frac{\partial \tilde{u}_j}{\partial x_i} \right] - \varepsilon_{kj} \frac{\partial \tilde{\varphi}}{\partial x_j} \right). \quad (6)$$



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• initial conditions, Dirichlet boundary conditions and Neumann boundary conditions are added:

$$\begin{aligned} \tilde{u}_i(., 0) = u_i, \quad x \in \Omega, \quad \tilde{u}_i = 0, \quad x \in \Gamma_u, \quad T_{ij}n_j = f_i, \quad x \in \Gamma_f, \quad i = 1, 2, 3, \quad (7) \\ \tilde{\varphi}(., 0) = \varphi, \quad \tilde{\varphi} = \varphi_D, \quad x \in \Gamma_\varphi, \quad D_k n_k = q, \quad x \in \Gamma_q, \end{aligned}$$

where

$$\Gamma_u \cup \Gamma_f = \Gamma, \quad \Gamma_u \cap \Gamma_f = \emptyset, \quad \Gamma_\varphi \cup \Gamma_q = \Gamma, \quad \Gamma_\varphi \cap \Gamma_q = \emptyset.$$

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  - \* system of ODEs for unknown values of  $\mathbf{u}$ ,  $\varphi$  in nodes of discretization results (our c++ code)

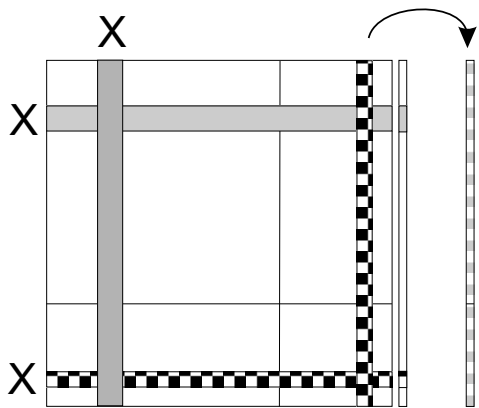
# Discretization of the problem, BC

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after introduction of Dirichlet boundary conditions, sub-matrices  $M$ ,  $K$  and  $E$  are symmetric and positive definite

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- eigenfrequencies can be computed by solving the generalized eigenvalue problem

$$\mathbf{A}\mathbf{X} = \lambda\mathbf{B}\mathbf{X} \quad (8)$$

with

$$\mathbf{A} = \begin{pmatrix} \mathbf{K} & \mathbf{P}^T \\ \mathbf{P} & -\mathbf{E} \end{pmatrix}, \quad \mathbf{B} = \begin{pmatrix} \mathbf{M} & 0 \\ 0 & 0 \end{pmatrix}, \quad \lambda = \omega^2,$$

A being symmetric and B being symmetric and positive semi-definite matrix

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$$K^*U = \lambda MU, \quad K^* = K - P^T E^{-1} P.$$

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- it loses the sparseness of the matrices; generalized Schur decomposition

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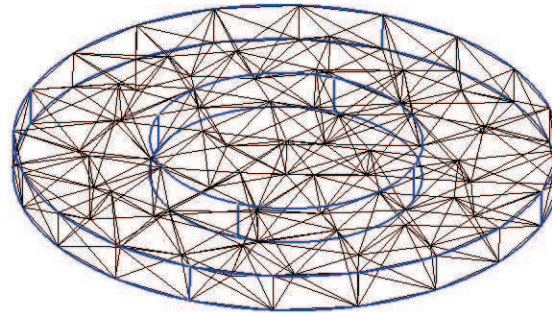
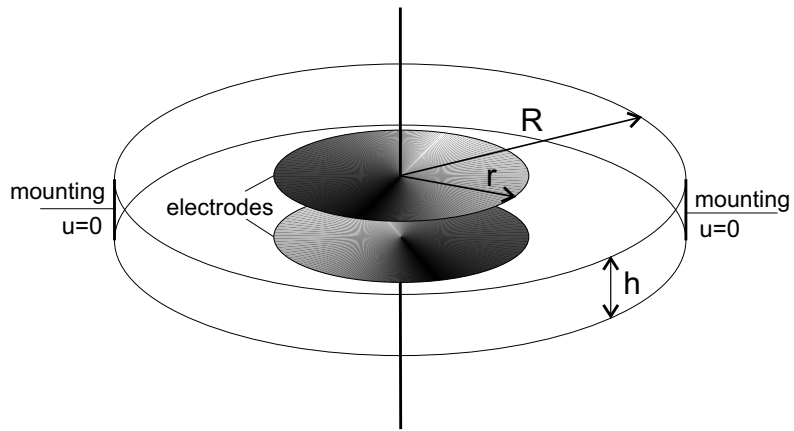
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# Numerical solution

- what is the shift:
- we can focus on the wanted part of the spectra - time and memory saving, higher precision

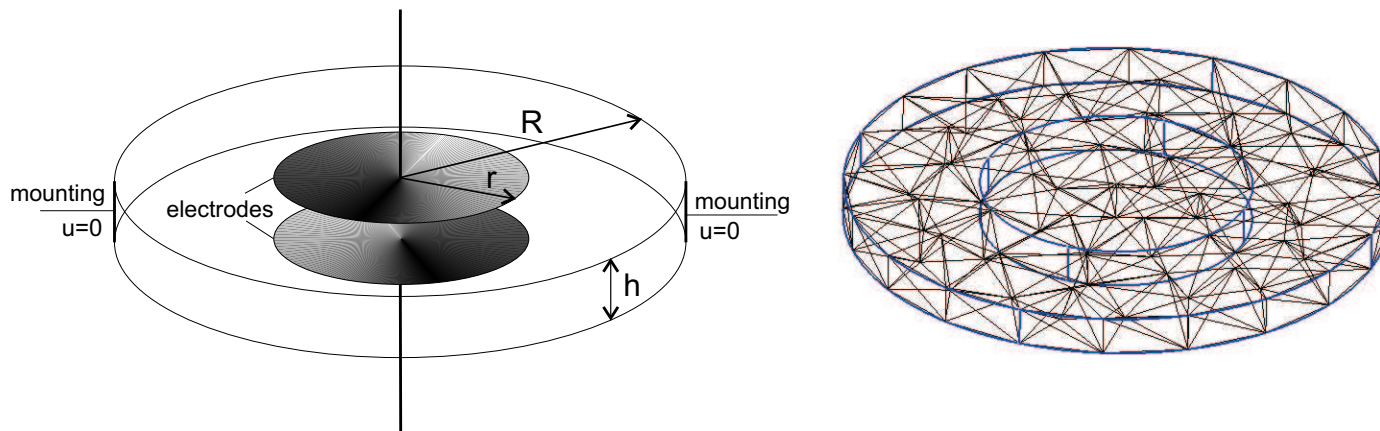
# Oscillation of planparallel quartz resonator

- shear vibration mode in  $x$  direction



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- three different samples

sample	R (mm)	r (mm)	h (mm)	res. freq.
1	7	3.5	0.333	5 MHz
2	3.975	2.5	0.168	10 MHz
3	3.475	1.5	0.0833	20 MHz

# Results

- comparison of measured and computed resonance frequencies:

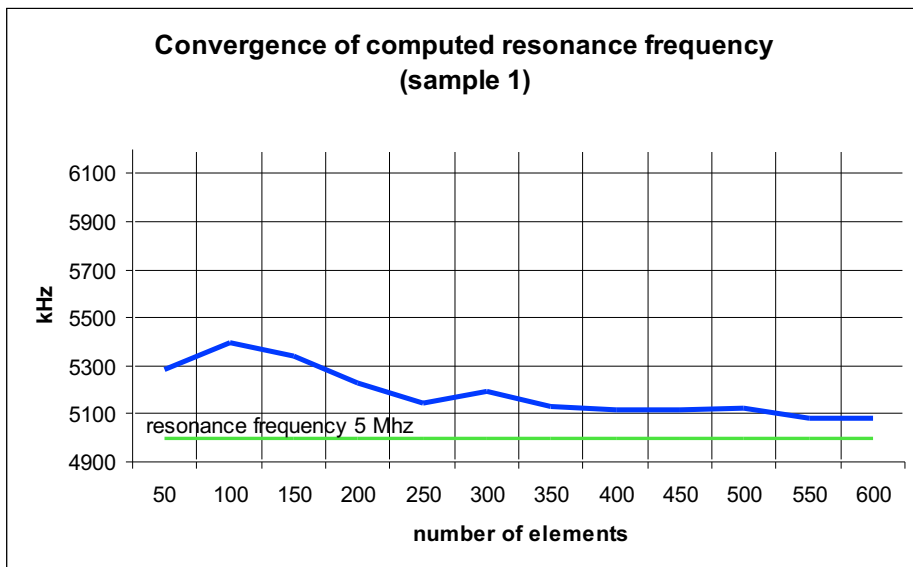
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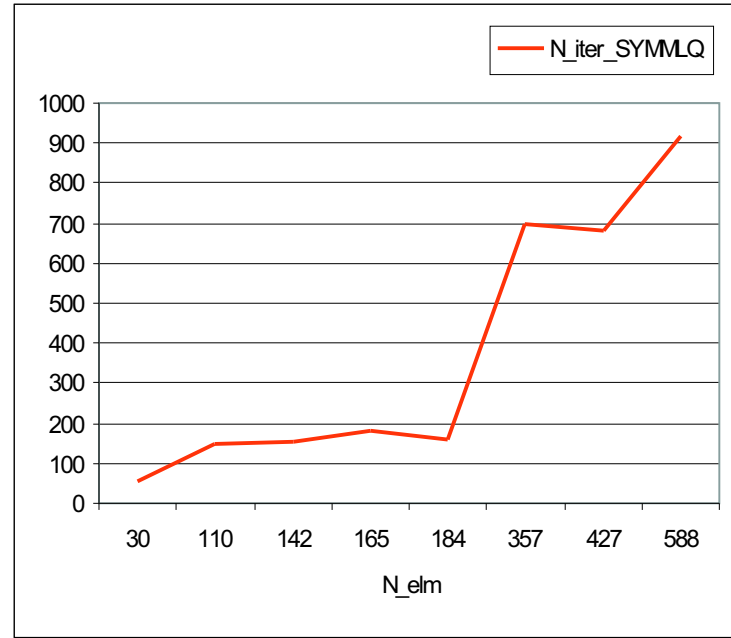
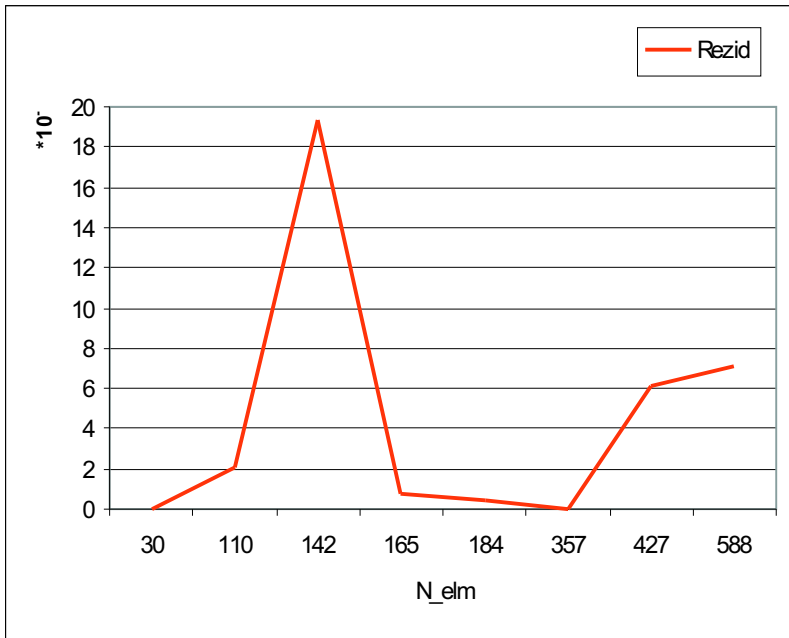
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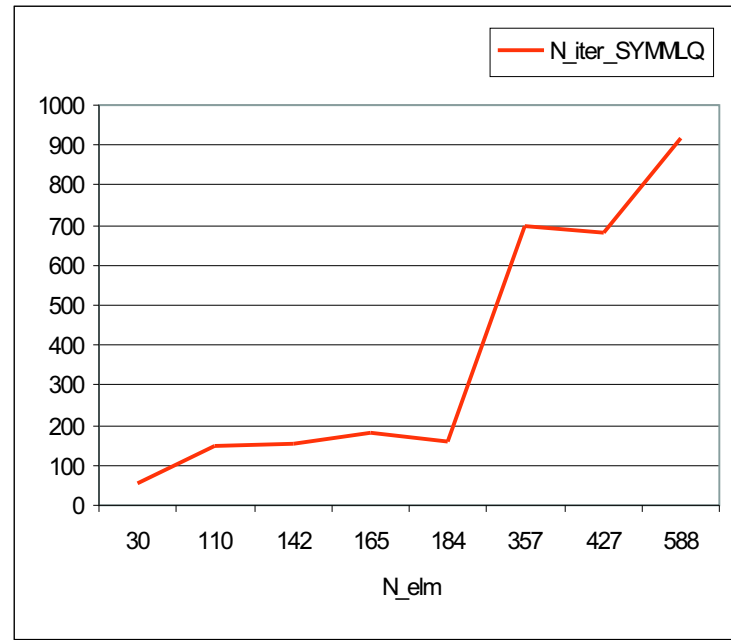
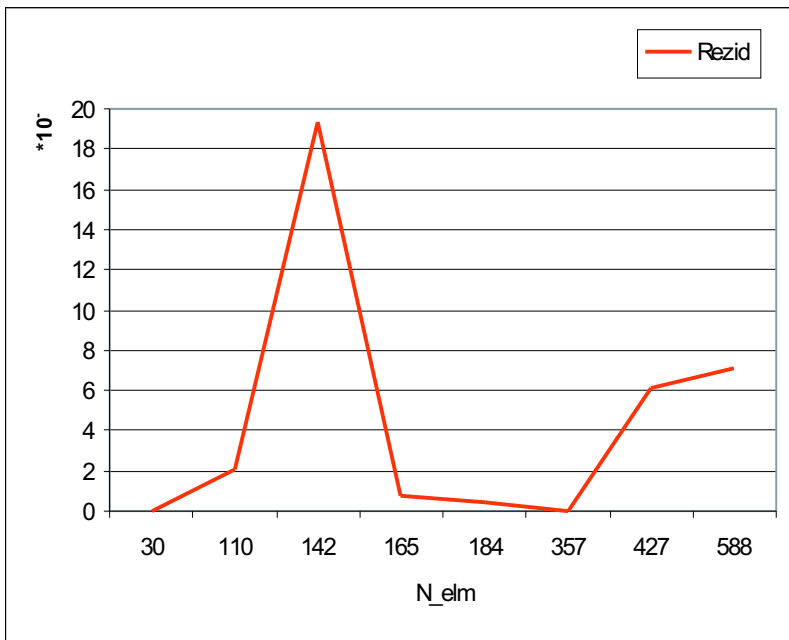
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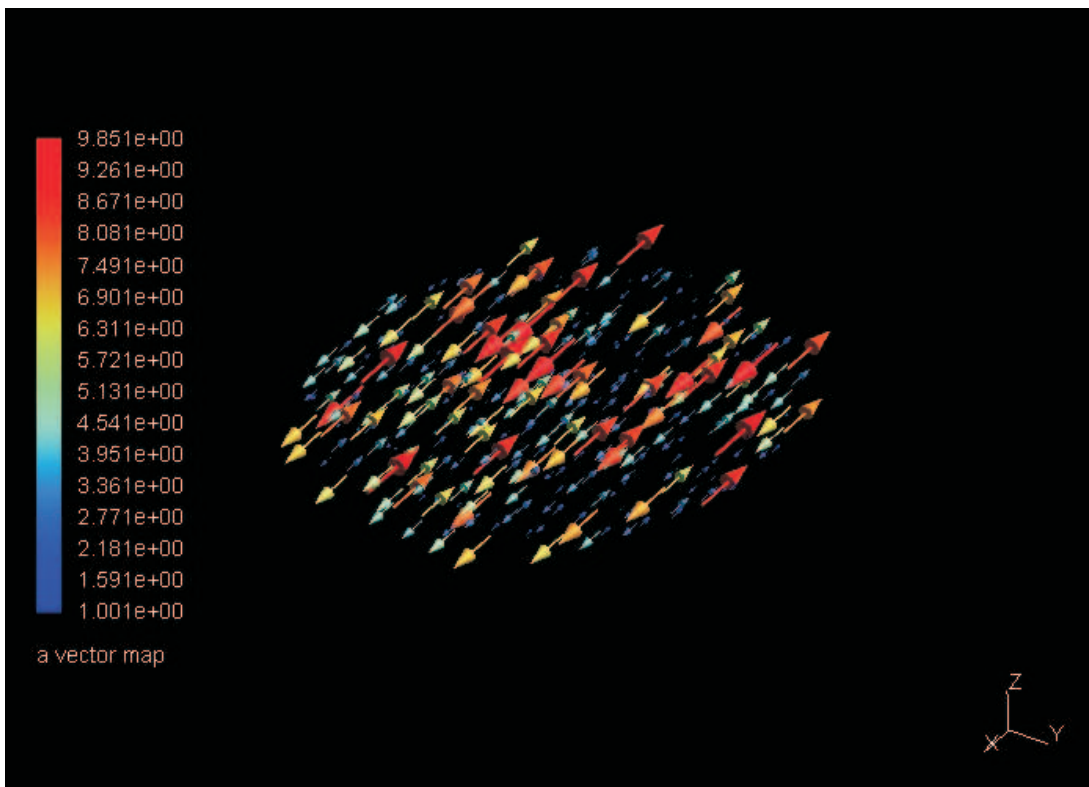
- rezidual about  $10^{-13}$  in worst case

# Postprocessing

- visualization in GMSH

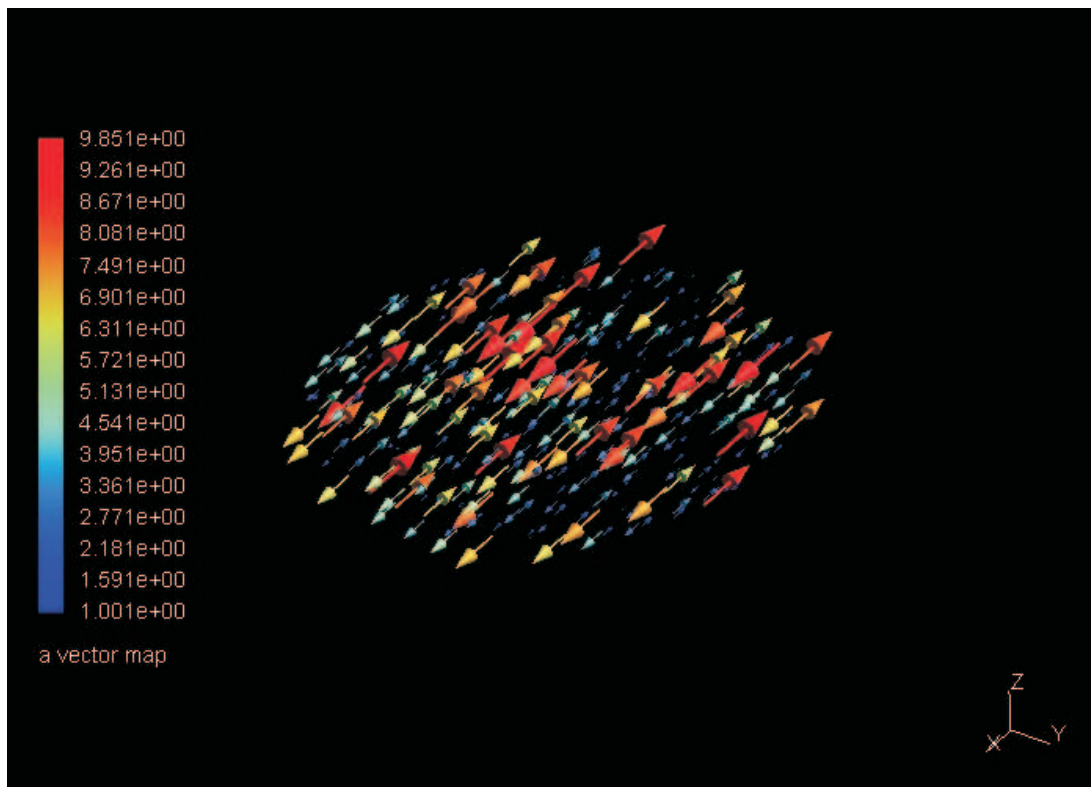
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- problems with recognition of vibrational modes - which are the right?

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physicians usually know, what should result and why; focus on practical problems